

SCHEMES OF METAL-WORKING PROCESSES AND THE RELATED TRIBOLOGICAL EQUATIONS OF FLUID MECHANICS

SHEME PROCESOV PREDELAVE KOVIN IN TRIBOLOŠKE ENAČBE MEHANIKE FLUIDOV ZANJE

Dušan Čurčija, Ilija Mamuzić

University of Zagreb, Faculty of Metallurgy Sisak, Aleja narodnih heroja 3, 44000 Sisak, Croatia
mamuzic@simet.hr

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We present a survey of the most frequently used equations for applications in cold drawing and rolling, for smooth and rough surfaces, for the effect of lubricant inertial forces, for more advanced theoretical solutions as well as the equations for cold drawing with a solid lubricant and the combination solid lubricant-emulsion. The compression processes are described using cylindrical coordinates. Also, the basic equations for the flowing of the lubricant on inclined planes related to screw rolling and for the forming of metals with fluids are given.

Key words: lubrication, metal forming Reynolds differential equation, Monte-Carlo method

Podan je pregled najbolj pogosto uporabljenih enačb pri hladnem valjanju in vlečenju, za gladke in hrapave površine, za vpliv vztrajnostnih sil, za bolj napredne teoretične rešitve in enačb za vlečenje s trdnim mazivom in kombinacijo trdo mazivo – emulzija. Tlačni procesi so opisani s cilindričnimi koordinatami. Podane so tudi osnovne enačbe za tok maziva na nagnjeni površini, ki se nanašajo na navojno valjanje in za oblikovanje kovine s fluidi.

Ključne besede: mazanje, preoblikovanje kovin, Reynoldova diferencialna enačba, metoda Monte Carlo

1 INTRODUCTION

The investigations and development of modern plastic working technology covers the following topics: physical modelling and simulation, computer simulation and characteristics and the behaviour of the material during processing.

The gradients representing the changes of temperature and mechanical stresses are greater for a greater per-pass (partial) deformation. In **Figure 1** the compression force F , the heat flow H , the deformation direction D and the rolling direction K for simple rolling

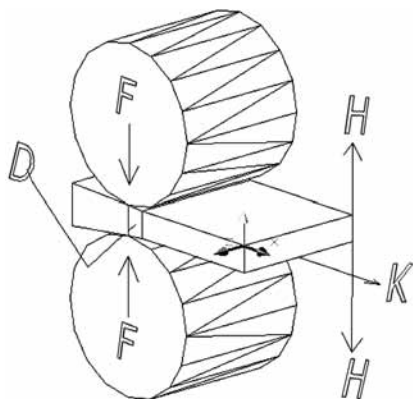


Figure 1: Directions of the gradients in a physical simulation of metal rolling¹

Slika 1: Smeri gradientov pri fizikalni simulaciji valjanja kovin¹

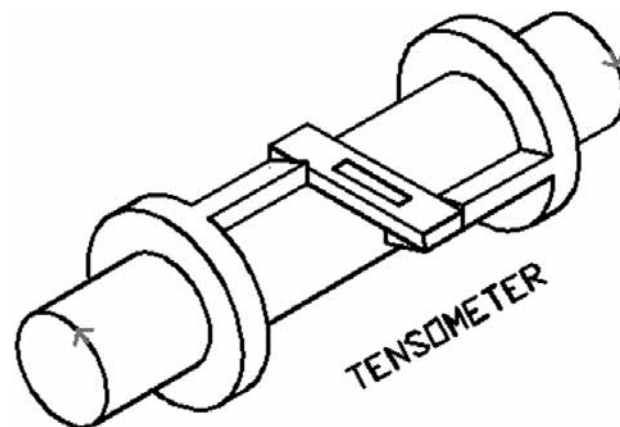


Figure 2: Torsionmeter²

Slika 2: Merilec torzije²

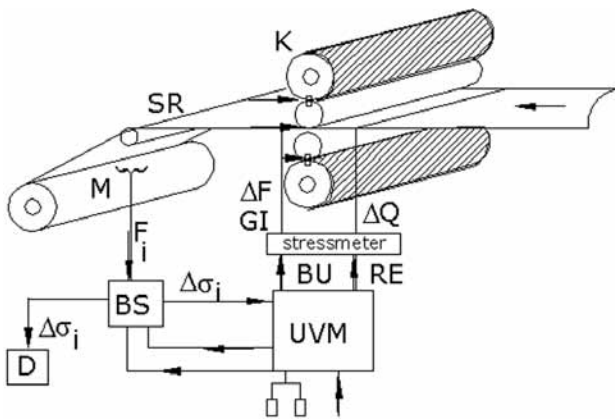


Figure 3: Measuring the surface stresses on a sheet's surface
Slika 3: Merjenje površinskih napetosti na traku

calibration as well as the regulation of the rolling gap for continuous rolling stands.

In **Figure 3** a scheme is given for measuring the stresses on the sheet surface with a stressmeter³.

2 FLUID MECHANICS

The concept of the boundary layer (**Figure 4**) was proposed by Prandtl in 1904. The thickness of the fluid layer (δ_x) can differ significantly from the flowing line 2. The layer has, however, a constant flow velocity. Below the laminar part of the layer 3, the flowing velocity (v) decreases and on the solid surface the fluid is at a standstill, ϕ is the boundary laminary layer, ω is the transition area and κ is the turbulent part of the boundary layer 1. The representation in **Figure 3** shifts the Navier-Stokes and Reynolds equations in the domain of velocity.

The use of emulsions for the plastic working of metals led to a significant lowering of production costs and to savings with expensive natural oils. In **Figure 5** the equilibrium is shown for the surface tension of a drop of light liquid on the surface of a heavier liquid:

$$\sigma_{12} = \sigma_{13} \cos\theta_2 + \sigma_{23} \cos\theta_1 \quad (1)$$

For $\theta_2 \rightarrow 0$ the adhesion work (W) is calculated using the Jung-Dupre equation

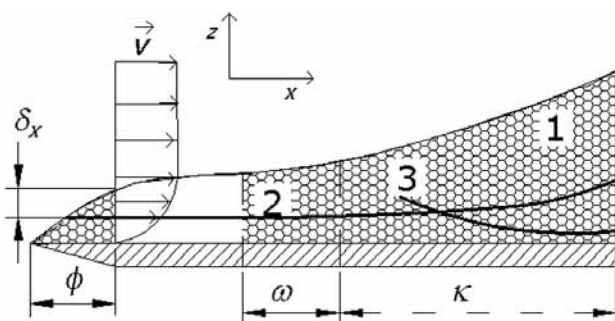


Figure 4: Boundary layer for the flow of fluid on the flat plane⁴
Slika 4: Mejni sloj za tok maziva na ravni površini⁴

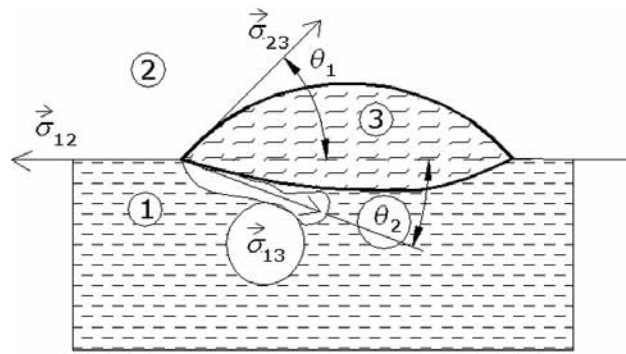


Figure 5: Equilibrium of the surface tension σ for a light liquid (3) on a heavier liquid (1) in air 2⁵

Slika 5: Ravnotežje površinske napetosti σ za lahko tekočino (3) na težji tekočini (1) in na zraku (2)⁵

$$W = \sigma_{23} (1 + \cos\theta_1) \quad (2)$$

Investigations of the use of equation (2) in metallurgy were carried out by Ju. P. Abdulov⁶. In a fluid mechanical metallurgical investigation different equations are used for the flat (**Figure 5**) and for the inclined plane (**Figure 6**).

The case of lubrication of a surface with vertical movement is met, also (**Figure 7**).

In this work we will examine the fluid friction (friction with hydrodynamic lubricant), for which Newton's law is applied:

$$F = z S v / h \quad (3)$$

where F is the friction force, z is the flowing capacity, S is the sliding surface, v is the velocity of the relative transfer, and h is the thickness of the lubricant layer.

For a description of the case of liquid friction in the plastic deformation of metals the Nady equation is used. Let us start with an analysis on the basis of **Figure 8**. The sheet of thickness h is covered with the lubricant layer $\epsilon(x)$ ahead of the section entering the deformation zone, for a wedge-shaped rolling gap a with the gap

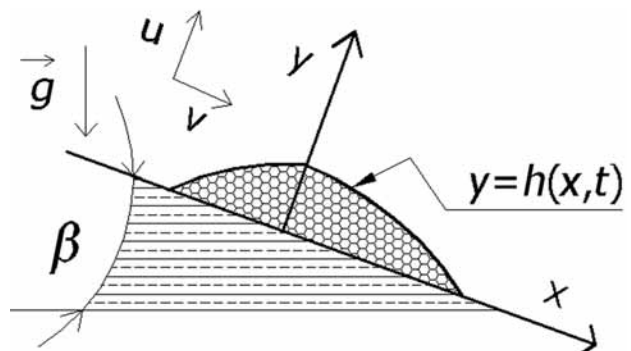


Figure 6: Shaping of a drop of liquid on an inclined plane⁷ where x, y are the Descartes coordinates; u, v are the corresponding flowing velocities; t is the time; g is the acceleration due to gravity; and β is the angle of inclination

Slika 6: Oblikovanje kapljice tekočine na nagnjeni površini x, y Descartesove koordinate; u, v hitrosti pretokov; t čas; g konstanta gravitacije; β kot nagiba

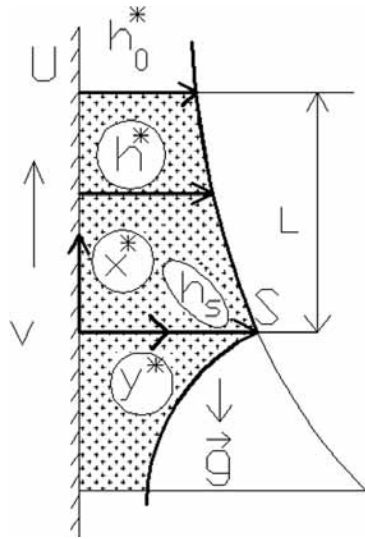


Figure 7: The dragging of fluid on a vertically moving metal surface⁸ where h_s is the thickness of the fluid layer on the stagnation line of a metal surface moving with the constant velocity of U , h_0^* is the thickness of the dragged fluid layer on the metal sheet, and v is the sheet velocity

Slika 7: Vlečenje maziva na površino s pokončnim gibanjem⁸ h_s – deblina sloja maziva na mirujoči točki metalne površine, ki se premika s stalno hitrostjo U , h_0^* – deblina sloja maziva, ki ga vleče kovinska površina, v – hitrost traka

angle α , sheet velocity v_0 , rolls velocity v_R and rolls radius R .

The Reynold's differential equations of fluid mechanics describing the representation in **Figure 8** are:

$$dp/dx = 6\mu(v_0 + v_R) / \varepsilon^2(x) - 12\mu Q / \varepsilon^3(x) \quad (4)$$

$$\tau = \mu(v_R - v_0) / \varepsilon(x) - (\varepsilon(x)/2) dp/dx \quad (5)$$

For $x = 0$ we have $\varepsilon(x) = \varepsilon_0$ in the entering section of the deformation zone. For the change of pressure gradient $dp/dx = 0$ the tangential stress in the lubricant layer (τ) is:

$$\tau = \mu(v_R - v_0) / \varepsilon(x) \quad (6)$$

In equation (6), attributed to Nady, μ is the lubricant dynamic viscosity, Q is the lubricant flow, $\varepsilon(x)$ is the lubricant layer thickness ahead of the section entering the deformation zone and dp/dx is the pressure gradient in the lubricant.

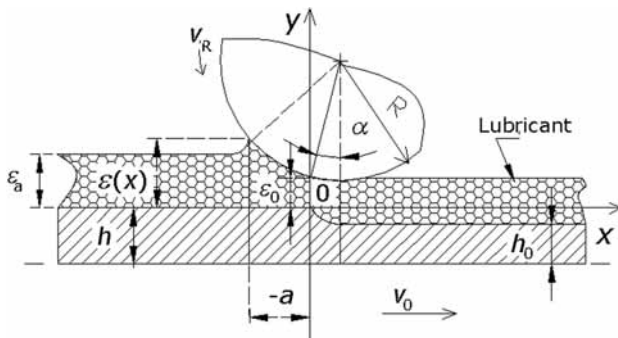


Figure 8: Cold rolling with a lubricant⁹

Slika 8: Hladno valjanje z mazanjem⁹

3 TECHNOLOGY OF THE PLASTIC WORKING OF METALS

This technology depends strongly on the quality of the technological lubricants used that:

- diminish the contact friction,
- remove the heat, cool the tool and diminish the wear,
- diminish the deformation resistance and the deformation work,
- diminish the sticking to the tool and keep the surface of the product clean.

The basic groups examined in this work are:

- liquid emulsions,
- fats and compounds,
- consistent lubricants,
- transparent – glass lubricants,
- powder lubricants,
- metallic lubricants.

The friction in cold deformation is, in principle, of the boundary type, and it is characterised with a great working pressure. The approaches in the development of the theory of friction are:

- geometrical, with the friction coefficient $\mu = \text{tg}\alpha$,
- molecular, with attraction based on a kinetical conception,
- deformation, based on the deformation work for a determined volume,
- a combination of different approaches.

The first calculations for the lubricant layer were by Mizuno¹⁰. According to Figure 8, the thickness of the lubricant layer is:

$$\varepsilon_0 = 3\mu_0\gamma(v_0 + v_R) / \alpha(1 - \exp(-p_0\gamma)) \quad (7)$$

with γ being the piezocoefficient lubricant viscosity, p_0 the rolling pressure, α the rolling angle, μ_0 the lubricant viscosity at atmospheric pressure, v_0 and v_R the working velocities of the tool and the rolling.

Also, new solutions were suggested, for example, Perlina, Grudeva and Kolmogorova for the technology of the cold drawing of metals,¹¹ according to **Figure 9**. The tube **3** moves with a velocity v_0 through the matrix **1** with the entering gap ψ ; it is covered with the lubricant **2** of thickness ε in the entrance section of the deformation zone.

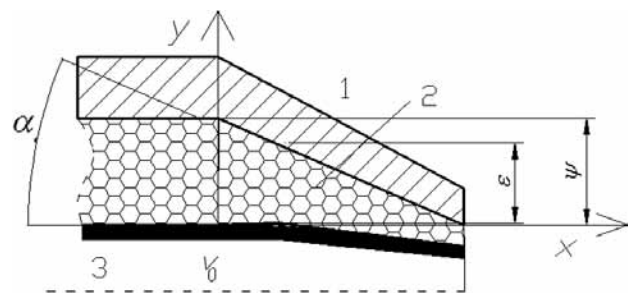


Figure 9: Cold drawing of metals with lubricant¹¹

Slika 9: Hladno vlečenje z mazanjem¹¹

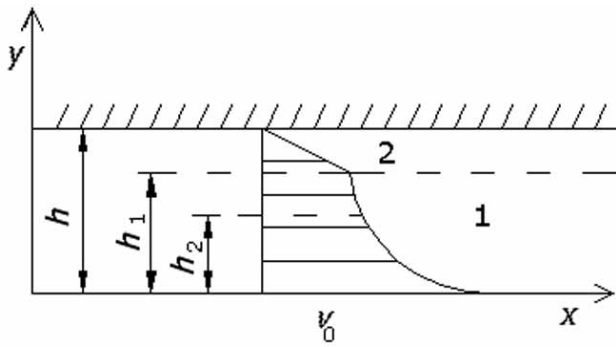


Figure 10: Distribution of velocity for the drawing of tubes with fat lubricant¹²

Slika 10: Porazdelitev hitrosti pri vlečenju cevi z masnim mazivom¹²

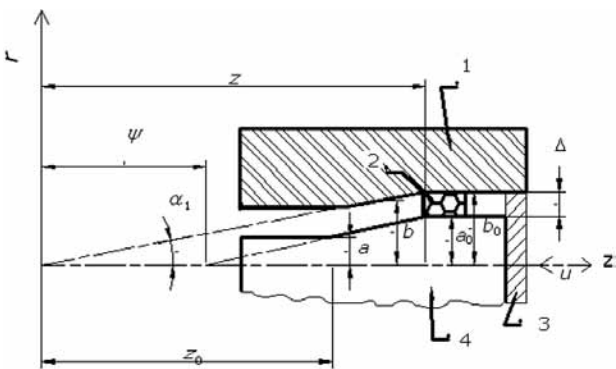


Figure 11: Pressing of metals¹³

Slika 11: Prešanje kovin¹³

The calculation is more complex for the case of combined liquid-solid lubrication. In Figure 10 the solid lubricant is the part 1 and the emulsion is the part 2. For the case in Figure 10 the maximum velocity of the emulsion is approximately 0.4 of the rolling velocity¹².

The pressing plastic deformation would be impossible without lubricant. The mathematical modelling in cylindrical coordinates is based on the scheme in Figure 11, with 1 being the round matrix, 2 the lubricant, 3 the mandrel, 4 the pressed metal and u the pressing velocity.

The forming with hydraulic fluid at the pressure 2 occurs over the membrane 1 (Figure 12). The liquid can have the role of either the matrix or of the extractor. For this process, a smaller number of toolings is used, the

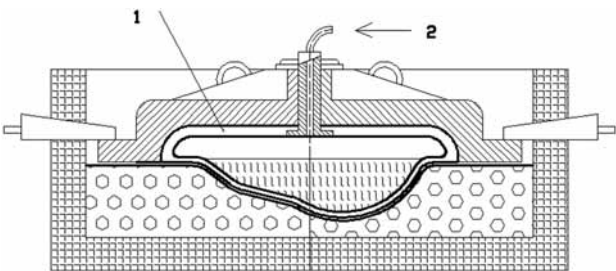


Figure 12: Hydraulic forming of a sheet

Slika 12: Hidravlično oblikovanje traka

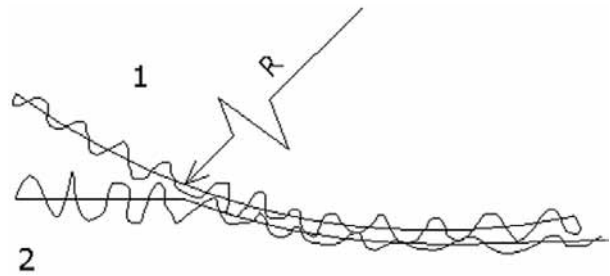


Figure 13: Uniform roughness of the rolls 1 and the sheet 2 surface¹⁴
Slika 13: Enakomerna hrpavost površine valja 1 in površine traka 2¹⁴

production costs are lower and complex forms are achieved more easily than when using conventional deep drawing.

The use of computers enabled us to also consider the surface roughness in the calculations (Figure 13) and the inertia of the lubricant with a great metal deformation velocity. In Table 1 are the differential equations for the average roughness.

The development of mathematical calculations for Pilger rolling are in the initial phase because of the complexity of the working surface of the Pilger rolls (Figure 14).

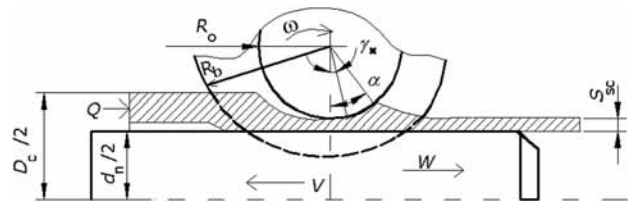


Figure 14: Scheme of Pilger rolling¹⁵, where v is the rolling direction, w is the direction of the tube D_C movement, α is the gripping angle, ω is the constant angle rotation of the Pilger rolls, γ_x is the angle of the neutral section, R_0 and R_b are the radii of the rolls' calibers, $d_n/2$ is the mandrel radius, S_{SC} is the thickness of the tube wall and Q is the direction of the material flow.

Slika 14: Shema Pilgerjevega valjanja: v – smer valjanja, w – smer cevi, D_C smer gibanja, α – kot prijema, ω – constantna kotna hitrost Pilgerjevih valjev, γ_x – kot nevtralnega prereza, R_0 in R_b – polmera kalibrov valjev, $d_n/2$ – polmer trna, S_{SC} – debelina stene cevi in Q – smer toka materiala

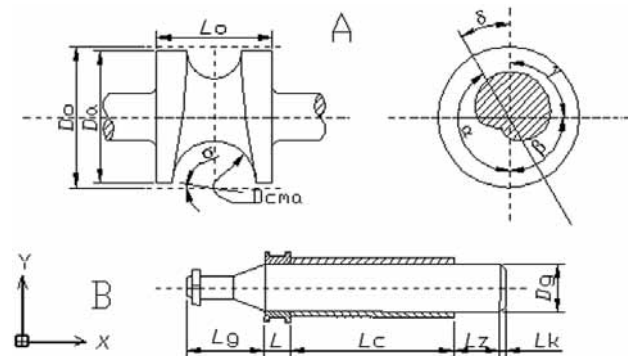


Figure 15: Elements of the Pilger stand: A is the roll, B is the mandrel¹⁶

Slika 15: Elementi Pilgerjevega ogrodja: A – valj, B – trn¹⁶

Table 1: The most frequently used differential equation of fluid mechanics applied for the description of the lubricant behaviour for different metal working processes

Tabela 1: Najbolji pogosto uporabljene enačbe in mehanike loma za opis vedenja maziva pri različnih procesih preoblikovanja kovin

Equation	Figure
<p>1. Smooth surface of the roll and of the metal worked (rolling, drawing, wire drawing)</p> $\partial p/\partial x = \mu \partial^2 v_x/\partial y^2; \partial p/\partial y = 0; \tau = \mu(v_R - v_0)/\varepsilon(x) - (\varepsilon(x)/2) dp/dx$ $\partial p/\partial z = \mu \partial^2 v_z/\partial y^2; \partial v/\partial x + \partial v/\partial y + \partial v/\partial z = 0$ <p>where v_z, v_x are the corresponding lubricant velocities, $\varepsilon(x)$ is the lubricant-layer thickness, dp/dx is the pressure gradient, τ is the tangential stress, μ is the lubricant dynamic viscosity, and v_R and v_0 are the working velocities for the tool and the material</p>	8 9
<p>2. Average roughness of the tool and of the material</p> $[dp/dx] = 6\mu(v_0 + v_R) \{ [1/\varepsilon^2(x_0)] - [1/\varepsilon_0^2] / [1/\varepsilon_0^3] \cdot [1/\varepsilon^3(x_0)] \}$ <p>$[]$ is the operator of the mathematical probability, $\varepsilon(x_0)$ is the random lubricant layer thickness, depending on the roughness of the tool and of the material, ε_0 is the lubricant-layer thickness in the access section of the zone of metal deformation</p>	14
<p>3. Sheet oiling</p> $H^3 d^3 H / Cadz^3 - (\gamma Ca)^{3/2} (T/5)(H^2 - 2H_s^2/3) dH/dz + (3H - H_s - T^2 H^3) = 0$ $H_s = 3 - T^2; H = 1 + \alpha; dH/dz = -c\alpha; d^2 H/dz^2 = c^2 \alpha; \alpha = A \exp(-cz); z = x^*/h^*$ $Ca = \mu U/\sigma; T = h_0^* (\rho g/\mu U)^{1/2}; \gamma = \sigma(v^4 g)^{-1/3} \rho; H = h^*/h_0^*$ <p>h_0^* is the ordinate of the free liquid surface, H is the dimensionless ordinate of the free surface, T is the dimensionless thickness h^*/h_0^* of the layer dragged on the metal surface, U is the velocity of the sheet withdrawal, z is the coordinate, v is the kinematical viscosity, and σ is the surface tension</p>	7
<p>4. Lubricant shaping on an inclined surface (inclined bending rolling)</p> $\partial p/\partial x = \mu \partial^2 u/\partial x^2 + \rho g \sin \beta - \partial \Phi/\partial x$ $\partial p/\partial y = -\rho g \cos \beta - \partial \Phi/\partial y; \partial h/\partial t + \mu \partial h/\partial x = v$ <p>Shaping of a drop on the horizontal plane (cylindrical coordinates)</p> $\partial p/\partial r = \mu \partial^2 v_x/\partial x^2$ <p>$\partial p/\partial r$ is the cylindrical coordinate system, Φ is the potential of the diffusion forces resulting from the interaction of lubricant molecules and the metal surface</p> $\Phi \approx 10^{-20} ((\text{tg} \alpha)^2 - \alpha^2)/h^3; t$ is the flowing time for a drop of lubricant; v is the velocity	6 18
<p>5. Metal pressing (extrusion), cylindrical coordinates</p> $(1/r)(\partial/\partial r(r \partial v_r/\partial r)) = (1/\mu) \partial p/\partial z$ <p>μ_t = the lubricant viscosity, depending on the temperature and pressure according to the Barussa equation.</p>	11
<p>6. Tube drawing with fat lubricant</p> $\tau_1 = -\tau_0 - dp/dx(h_2 - y);$ $\tau = \tau_0 + K \gamma_0 ^{m-1} \gamma_0$ $v = (h_2 - y)^{c+1}/(c+1) \cdot (1/K) (dp/dx)$ <p>τ_1, τ_0 are the critical tangential stresses at the boundary tool and worked piece, h is the gap height between the tool and the worked piece, γ is the worked piece velocity, K, m, c are the rheological characteristics of the fat.</p>	10
<p>7. Effect of inertia and of the smooth tool and worked piece surfaces</p> $\partial p/\partial x = 6\mu(v_0 + v_R)/\varepsilon^2(x) + C_1 \mu/\varepsilon^3(x) + \rho \text{tg} \alpha (16v_0^2 \varepsilon^2(x) - C_1^2)/120 \varepsilon^3(x)$ $C_1 = k/2 - (k^2/4 + 2v_0 \varepsilon_0 (8v_0 \varepsilon_0 + 3k))^{1/2}; k = 120v/\text{tg} \alpha$ $\varepsilon(x) = \varepsilon_0 - \alpha x + x^2/2R - \alpha x^3/2R^2 + \dots$ <p>α is the gripping or drawing angle, R is the roll's radius, v_0, v_R are the working velocities for the tool and the worked piece, and v is the kinematical viscosity</p>	8
<p>8. New approaches to the mathematical modelling (rolling of metals)</p> $dk/d(\varphi/\alpha) = 6W(\Delta h/\varepsilon_0)^2(H_{0S} - H_{HS})/H_{HS}^3 e^{Mk}; W = \mu_0(v_0 + v_R)/\sigma_T \Delta h \alpha$ $H_{HS} = \Delta h/2\varepsilon_0 [(\varphi/\alpha)^2 - 1] + H_{0S} [C_1/\Delta_1(\varphi/\alpha - (1 - \Delta_1)) + k] +$ $+ R_{za}/2\varepsilon_0 \sin[2\pi(\varphi/\alpha - (1 - \Delta_1))/C_{a0}\Delta_1 + C_{a1}] +$ $+ R_{zn}/2\varepsilon_0 \sin[2\pi(\varphi/\alpha - (1 - \Delta_1))/C_{n0}\Delta_1 + C_{n1}] -$ $- (1 + R_{za}/2\varepsilon_0 \sin C_{a1} + R_{zn}/2\varepsilon_0 \sin C_{n1})k + 1$ <p>where C_{a1}, C_{n1} are the roughness of the rolls and the sheet, C_1 is the coefficient considering the shape of the wedge-shaped lubricant gap (zone 1), Δh is the absolute reduction, φ is the local angle in the deformation zone, α is the gripping angle, μ_0 is the dynamical viscosity at air pressure, R_{zn}, R_{za} are the sheet and rolls roughness, $\Delta_1 = \sigma_T/(2\delta E_E)$, σ_T is the module of flowing, δ is the relative reduction, E_E is the module of elasticity, $k = p/\sigma_T$, p is the rolling pressure, $M = \theta \sigma_T$, θ is the piezocoefficient of viscosity, e is the base of the natural logarithm, $H_{0S} = \varepsilon_1/\varepsilon_0$, $H_{HS} = \varepsilon/\varepsilon_0$, ε_0 is the thickness of the lubricant layer at the access of the deformation zone, C_{a0}, C_{n0} are the roughness amplitudes for the rolls and the sheet, v_0 and v_R are the working velocities for the rolls and the sheet</p>	20

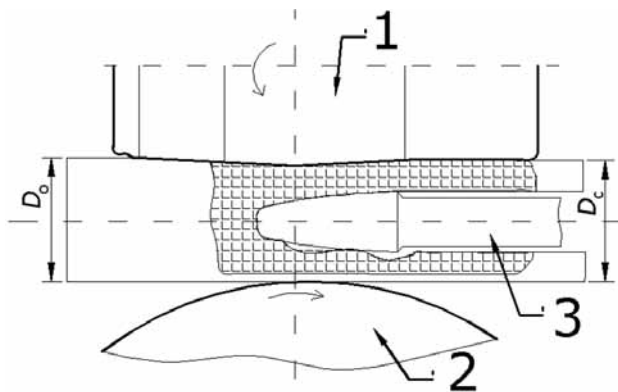


Figure 16: Scheme of the drilling of the rolling in a modern bending stand¹⁷

Slika 16: Shema prebijanja valjanca v modernem upogibnem ogrodju¹⁷

Pilger rolling is a periodic process and it is one of the most complex processes of plastics, since it deforms metals and combines the characteristics of rolling and forging with metal forming in the caliber of the changing section (Figure 15).

The Pilger rolling stand in Figure 15 has three parts inside the working caliber:

- the front part, where the basic metal deformation is achieved, α ,
- the polishing part, where the final tube size is achieved, β ,
- and the longitudinal part, where the transition from the polishing to the final barren part occurs, γ .

The methods of the plastic deformation of metal between the drawing, rolling, and pressing with already developed calculations of the behaviour of the lubricant layer and the insufficiently investigated Pilger rolling are:

- the drilling on the Diescher disc (Figure 16),
- bending (inclined) drilling (Figure 17),
- three-rolls rolling stands rolling (Figure 18).

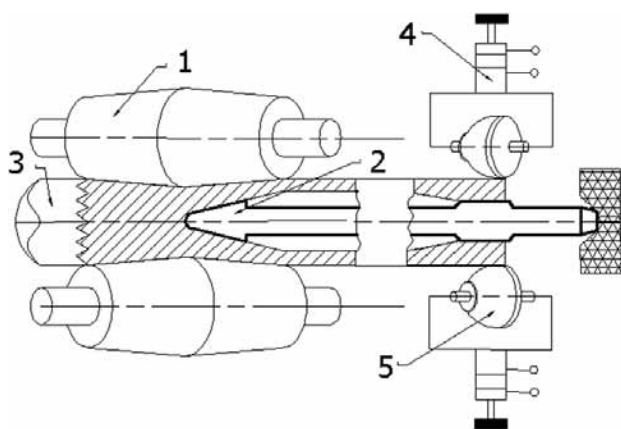


Figure 17: Scheme of the drilling stand for bending rolling with barrel-shaped rolls¹⁸

Slika 17: Shema prebijalnega ogrodja za upogibno valjanje s sodastimi valji¹⁸

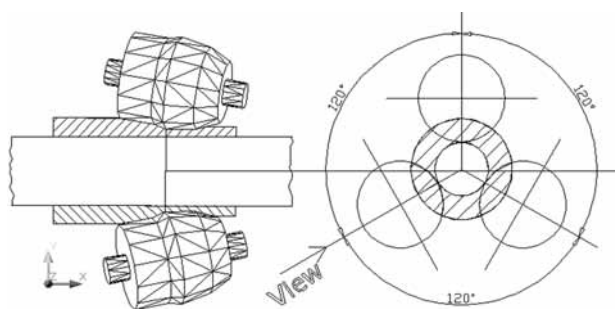


Figure 18: Scheme of the tube deformation in the three-rolls high rolling stand¹⁹

Slika 18: Shema deformacije cevi v triovaljalnem ogrodju¹⁹

The drilling mandrel (3) advances through the pierced round of diameter D_0 . Above the rolling is the working stand (1) and below it is the Diescher disc (2).

The mandrel 2 drills the rolling 3 with the rotation of the barrel-shaped rolls 1 with support from the hydraulic cylinders 4 and the barrel-shaped rolls 5.

The working rolls of the three-rolls high rolling stand are set at an angle of 120° . The gripping angle is selected in the range 0° to 10° and the rolling angle in the range 3° to 7° . Specific to the stands is the shape of the working rolls that increase the regularity of the metal

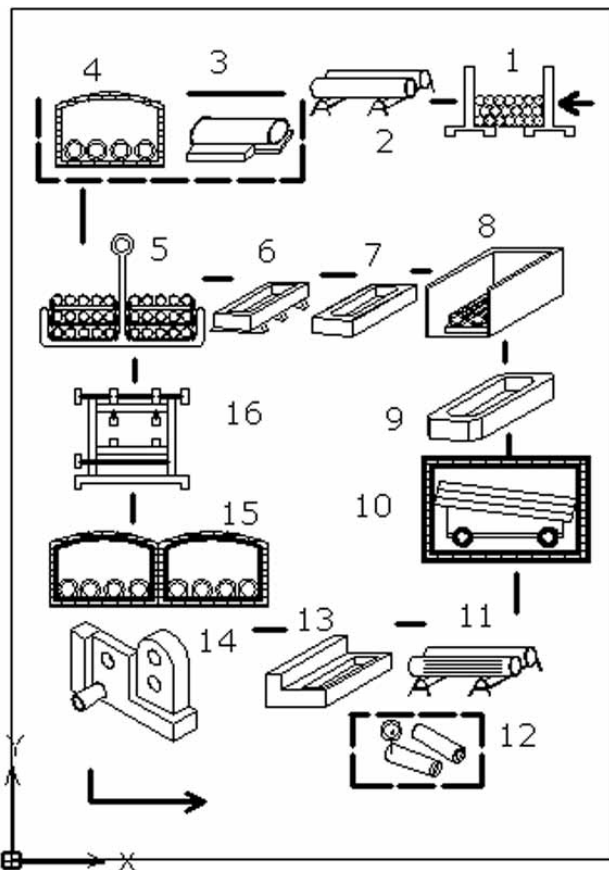


Figure 19: Technological scheme of the manufacturing of tubes with cold rolling²⁰

Slika 19: Tehnološka shema za izdelavo cevi s hladnim valjanjem²⁰

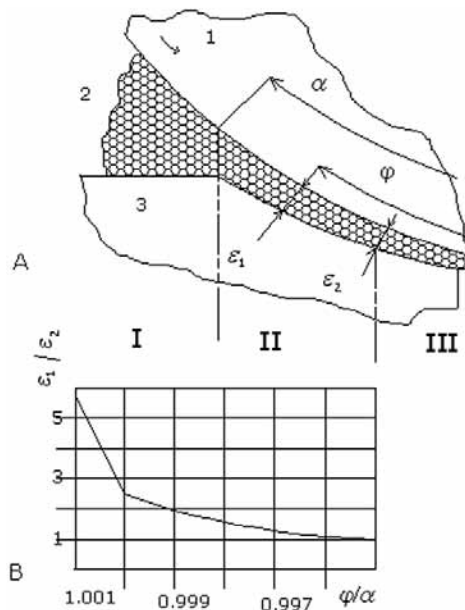


Figure 20: Mathematical modelling of the rolling with lubricant and the approach to the deformation zone²⁵
Slika 20: Matematično modeliranje valjanja z mazivom in približek za zono deformacije²⁵

flow and the tube quality. (1, the gripping cone; 2, the rolls ridge; 3, polishing cone; and 4, the release cone).

In **Figure 19** the technological scheme of the manufacturing of tubes with cold rolling is shown with: 1) billets storehouse; 2) inspection; 3) cutting of tube ends; 4) heat treatment; 5) collecting of tubes in packets; 6) decapping; 7) rinsing with hot water; 8) rinsing with cold water; 9) neutralization; 10) drying; 11) inspection; 12) repairing; 13) lubrication; 14) rolling on the cold Pilger stand; 15) intermediate heat treatment; 16) straightening.

5 DIFFERENTIAL EQUATIONS

In **Table 1** the equations describing the lubricant behaviour for different metal-working processes are given.

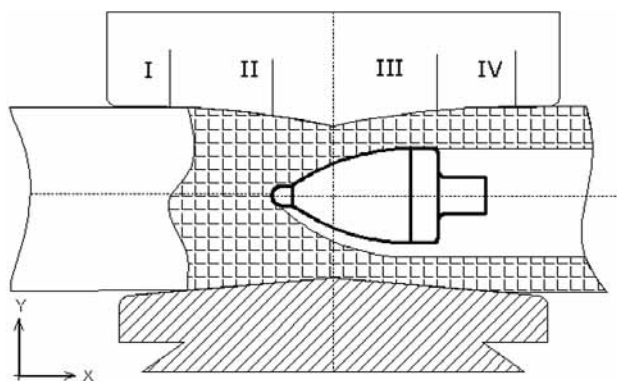


Figure 21: Deformation zone by bending rolling
Slika 21: Zona deformacije pri upogibnem valjanju

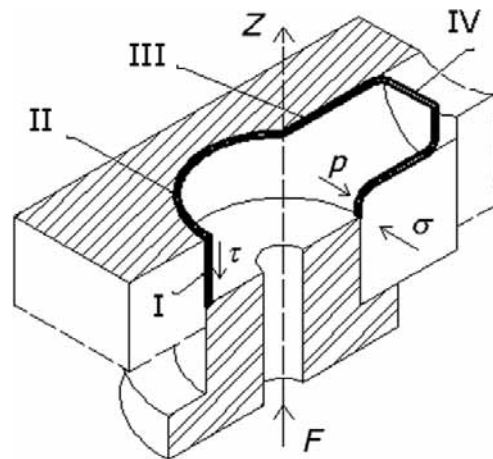


Figure 22: Forming of the T-shaped tube end (F is the axial force, p is the fluid pressure, σ and τ are the normal and tangential stresses)
Slika 22: Oblikovanje konca cevi v obliko T (F – aksialna sila, p – pritisek tekočine, σ in τ – normalne in tangencialne napetosti)

The use of lubricant in the plastic-deformation processes has increased greatly the working velocity, which required a consideration of the inertia effects in the calculations of the lubricant layer²⁶. Computer calculations made it possible to also consider the effects of roughness^{27,28}, the mathematical modelling based on the Fourier series²⁹ and the reduction in lubricant use, considering the shape of the lubricant wedge ahead of the access section of the zone of plastic deformation³⁰ (**Figure 20**).

In parallel with the investigations of the lubrication for the plastic working of metals^{31,32}, more efficient lubricants were also developed^{33,34}. It is to be expected that fluid mechanics will also be applied for a description of the lubricant behaviour in the processes of bending rolling, shown in **Figure 21**.

On the longitudinal section of the deformation zone of bending rolling the following zones are distinguished:

1. the drilling zone (from plane I to plane II),
2. the rolling on the mandrel zone (from plane II to plane III),
3. the reduction of the worked piece in the absence of the mandrel zone (from plane III to plane IV).

The application of the Reynolds' differential equation will probably start with the zone of rolling on the mandrel.

New findings of the forming of tubes with a fluid are presented in ref.³⁶ with the forming of the T-shaped end tubes shown in **Figure 22**.

- Four characteristic zones are distinguished:
- I – the zone of the main tube (flat stress-state)
 - II – the zone of the tube translating into drainage (volume stress-strain state)
 - III – the drainage zone (pressure and stretching stresses)
 - IV – the drainage peak zone (pressure and stretching stresses)

6 CONCLUSION

The use of fluid mechanics for the calculation of the behaviour of the lubricant layer in the metal deformation zone for most of the metal working processes has greatly increased with the application of computers. In the article a survey is given over the scheme of different metal-working processes and of the differential equations used for the description of the lubricant behaviour. Mostly, the derived equations are based on the Reynolds' differential equation and only some are also based on the Navier-Stokes' equation.

In modern methods of modelling of the lubricated plastic deformation of metals supplementary equations are also included to better consider the parameters of the working process. Actually, the calculations are applied mostly for the processes of the cold drawing and the rolling of metals³⁵, while for the Pilger processing they are being developed.

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